

LA-UR-16-24113

Approved for public release; distribution is unlimited.

Title: Water Solubility of Plutonium and Uranium Compounds and Residues at TA-55

Author(s): Reilly, Sean Douglas
Smith, Paul Herrick
Jarvinen, Gordon D
Prochnow, David Adrian
Schulte, Louis D.
DeBurgomaster, Paul Christopher
Fife, Keith William
Rubin, Jim
Worl, Laura Ann

Intended for: Report

Issued: 2016-06-13

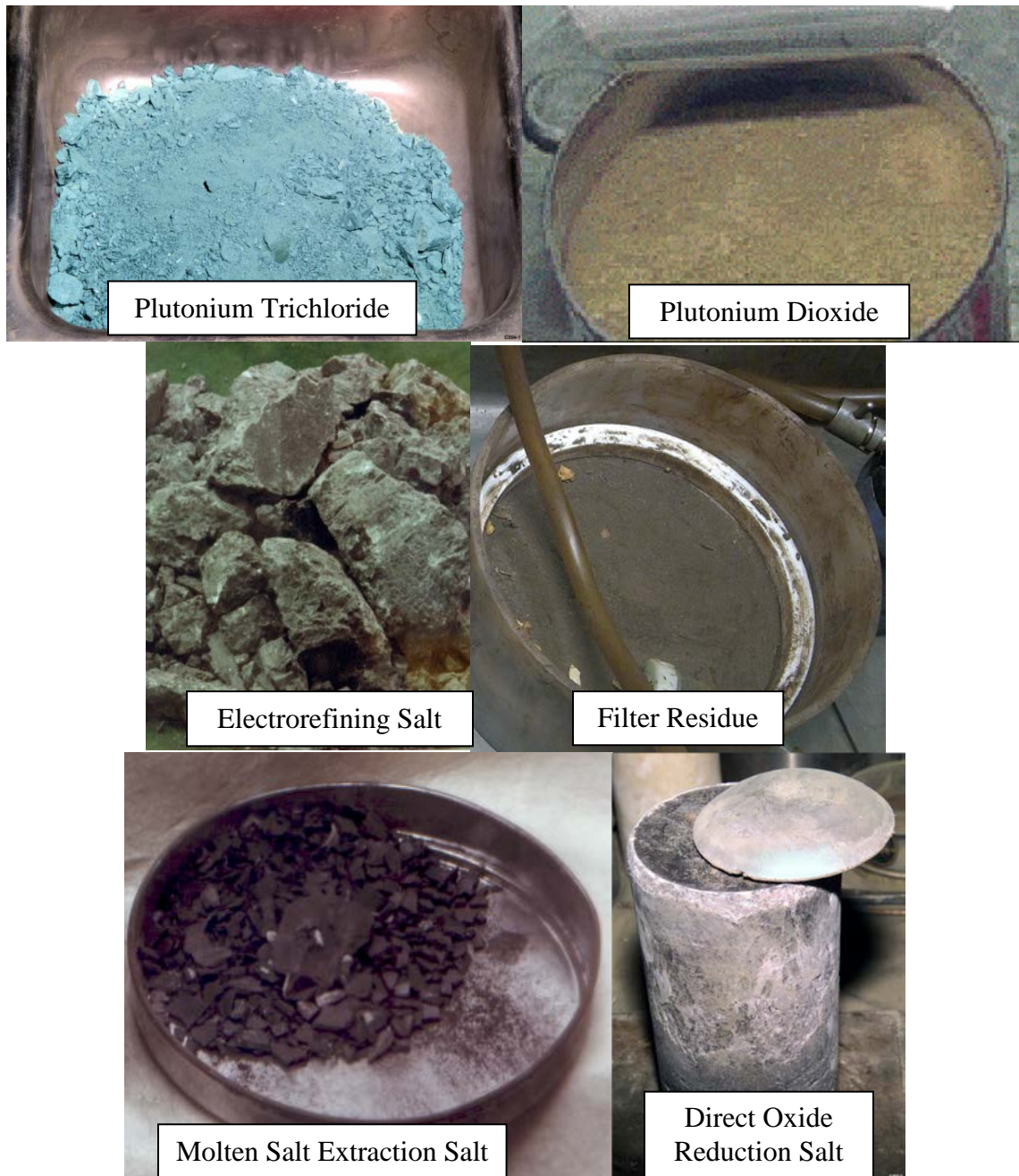
Disclaimer:

Los Alamos National Laboratory, an affirmative action/equal opportunity employer, is operated by the Los Alamos National Security, LLC for the National Nuclear Security Administration of the U.S. Department of Energy under contract DE-AC52-06NA25396. By approving this article, the publisher recognizes that the U.S. Government retains nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or to allow others to do so, for U.S. Government purposes. Los Alamos National Laboratory requests that the publisher identify this article as work performed under the auspices of the U.S. Department of Energy. Los Alamos National Laboratory strongly supports academic freedom and a researcher's right to publish; as an institution, however, the Laboratory does not endorse the viewpoint of a publication or guarantee its technical correctness.

Water Solubility of Plutonium and Uranium Compounds and Residues at TA-55

Sean D. Reilly (C-NR), Paul H. Smith (NPI-2), Gordon D. Jarvinen (NSEC),
David A. Prochnow (NPI-2), Louis D. Schulte (MET-1), Paul C. Deburgomaster (MET-1),
Keith W. Fife (MET-1), Jim Rubin (MET-1), Laura A. Worl (IPM)

June 10, 2016



Water Solubility of Plutonium and Uranium Compounds and Residues at TA-55

Executive Summary

Understanding the water solubility of plutonium and uranium compounds and residues at TA-55 is necessary to provide a technical basis for appropriate criticality safety, safety basis and accountability controls. Individual compound solubility was determined using published solubility data and solution thermodynamic modeling. Residue solubility was estimated using a combination of published technical reports and process knowledge of constituent compounds. The scope of materials considered includes all compounds and residues at TA-55 as of March 2016 that contain Pu-239 or U-235 where any single item in the facility has more than 500 g of nuclear material. This analysis indicates that the following materials are not appreciably soluble in water: plutonium dioxide (IDC=C21), plutonium phosphate (IDC=C66), plutonium tetrafluoride (IDC=C80), plutonium filter residue (IDC=R26), plutonium hydroxide precipitate (IDC=R41), plutonium DOR salt (IDC=R42), plutonium incinerator ash (IDC=R47), uranium carbide (IDC=C13), uranium dioxide (IDC=C21), U_3O_8 (IDC=C88), and uranium filter residue (IDC=R26). This analysis also indicates that the following materials are soluble in water: plutonium chloride (IDC=C19) and uranium nitrate (IDC=C52). Equilibrium calculations suggest that $PuOCl$ is water soluble under certain conditions, but some plutonium processing reports indicate that it is insoluble when present in electrorefining residues (R65). Plutonium molten salt extraction residues (IDC=R83) contain significant quantities of $PuCl_3$, and are expected to be soluble in water. The solubility of the following plutonium residues is indeterminate due to conflicting reports, insufficient process knowledge or process-dependent composition: calcium salt (IDC=R09), electrorefining salt (IDC=R65), salt (IDC=R71), silica (IDC=R73) and sweepings/screenings (IDC=R78). Solution thermodynamic modeling also indicates that fire suppression water buffered with a commercially-available phosphate buffer would significantly reduce the solubility of $PuCl_3$ by the precipitation of $PuPO_4$.

Table of Contents

1	Introduction	1-1
1.1	Background.....	1-1
1.2	Conditions of Criticality Concern.....	1-1
2	Computational Methods	2-1
3	Results and Discussion	3-1
3.1	Plutonium Compounds	3-1
3.1.1	Plutonium Chloride (C19).....	3-1
3.1.2	Plutonium Dioxide (C21).....	3-4
3.1.3	Plutonium Phosphate (C66)	3-5
3.1.4	Plutonium Tetrafluoride (C80).....	3-8
3.1.5	Plutonium Oxychloride	3-8
3.2	Plutonium Residues	3-9
3.2.1	Plutonium Calcium Salt (R09).....	3-9
3.2.2	Plutonium Filter Residue (R26)	3-10
3.2.3	Plutonium Hydroxide Precipitate (R41)	3-10
3.2.4	Plutonium Direct Oxide Reduction (DOR) Salt (R42)	3-11
3.2.5	Plutonium Incinerator Ash (R47).....	3-11
3.2.6	Plutonium Electrorefining (ER) Salt (R65)	3-12
3.2.7	Plutonium Salt (R71)	3-12
3.2.8	Plutonium Silica (R73)	3-12
3.2.9	Plutonium Sweepings/Screenings (R78).....	3-12
3.2.10	Plutonium Molten Salt Extraction (MSE) Salt (R83)	3-13
3.3	Uranium Compounds	3-14
3.3.1	Uranium Carbide (C13)	3-14
3.3.2	Uranium Dioxide (C21)	3-14
3.3.3	Uranium Nitrate (C52).....	3-14
3.3.4	Uranium U ₃ O ₈ (C88).....	3-14
3.3.5	Uranium Uranates	3-14
3.4	Uranium Residues.....	3-14

3.4.1 Uranium Filter Residue (R26)	3-14
3.5 Summary	3-14
4 Conclusions.....	4-1
5 References.....	5-1
6 Appendix 1. Derivation of Equilibrium Constants	6-1

List of Figures

Figure 1-1. Critical volumes of homogeneous water-moderated plutonium spheres. The points suggesting an intermediate curve apply to water-reflected $\text{Pu}(\text{NO}_3)_4$ solution with 1 M HNO_3 and 3.1% ^{240}Pu content of the plutonium (black and white figure and caption reproduced from LA-10860-MS). The blue and red lines show the solution volumes as a function of Pu density (kg/L Pu in solution) for various Pu element masses. The arrows indicate the approximate minimum critical volumes for the water reflected case.....	1-2
Figure 3-1. Plutonium Trichloride (C19 and C82)	3-1
Figure 3-2. Critical volumes of homogeneous water-moderated plutonium spheres (reproduced from LA-10860-MS). The red line plots the quantity of Pu that dissolves for a given volume of water (expressed as kg Pu/L H_2O on the x-axis for a given volume of water on the y-axis).	3-2
Figure 3-3. Speciation of 2,390 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.	3-3
Figure 3-4. Speciation of 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.	3-3
Figure 3-5. Plutonium Dioxide (C21).....	3-4
Figure 3-6. Critical volumes of homogeneous water-moderated plutonium spheres (blue line, reproduced from LA-10860-MS). The red line plots the quantity of Pu that dissolves for a given volume of water (expressed as kg Pu/L H_2O on x-axis for a given volume of water on y-axis). 3-4	3-4
Figure 3-7. Speciation of 2,450 g Pu as $\text{PuO}_2(\text{am, hyd})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.....	3-5
Figure 3-8. Critical volumes of homogeneous water-moderated plutonium spheres (reproduced from LA-10860-MS). The dotted red line shows the quantity of Pu that dissolves for a given volume of water (expressed as kg Pu/L H_2O on the x-axis for a given volume of water on the y-axis). The two red lines illustrate that the Pu solubility can be significantly reduced by adding 0.094 M K_2HPO_4 /0.006 M KH_2PO_4 buffer, and further reduced by adding 0.72 M K_2HPO_4 /0.28 M KH_2PO_4 buffer, resulting in the precipitation of PuPO_4	3-6

Figure 3-9. Speciation of 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added 0.094 M K_2HPO_4 /0.006 M KH_2PO_4 buffered water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis. 3-7

Figure 3-10. Speciation of 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added 0.72 M K_2HPO_4 /0.28 M KH_2PO_4 buffered water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis. 3-7

Figure 3-11 Critical volumes of homogeneous water-moderated plutonium spheres (blue line, reproduced from LA-10860-MS). The red line plots the quantity of Pu from PuOCl that dissolves for a given volume of water (expressed as kg Pu/L H_2O on x-axis for a given volume of water on y-axis). 3-8

Figure 3-12 Speciation of 2,390 g Pu as $\text{PuOCl}(\text{s})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis. 3-9

Figure 3-13. Plutonium filter residue (dissolution heel) from aqueous nitrate dissolution process. This is the material that remains undissolved and is subsequently collected by filtration after heating a plutonium residue in strong nitric acid solution. 3-10

Figure 3-14. Plutonium Direct Oxide Reduction (DOR) Salt (R42). The plutonium metal button product is pictured on top of the calcium salt cake..... 3-11

Figure 3-15. Plutonium Electrorefining (ER) Salt (R65)..... 3-12

Figure 3-16. Plutonium Molten Salt Extraction (MSE) Salt (R83). 3-13

List of Tables

Table 2-1. Chemical equilibria and equilibrium constants 2-1

Table 3-1. Summary of water solubility results..... 3-15

Acronyms and Abbreviations

Abbreviation	Term
DOR	Direct Oxide Reduction
ER	Electrorefining
IDC	Item Description Code
LANMAS	Local Area Nuclear Material Accountability Software
MSE	Molten Salt Extraction
NEA	Nuclear Energy Agency (OECD)

1 Introduction

1.1 Background

Understanding the water solubility of nuclear materials used at the TA-55 Plutonium Facility has significant implications for safety and security. For example, water-soluble fissile materials used in gloveboxes at TA-55 are required to be stored in water-resistant containers to prevent water intrusion and mitigate the risk of a criticality accident in the event of glovebox flooding due to an earthquake and subsequent fire. Knowledge of the water solubility is necessary to improve operational efficiency where the solubility assumption is overly conservative. Conversely, where there is a programmatic need to handle significant quantities of water-soluble fissile material, this knowledge is necessary to provide a technical basis for appropriate criticality safety controls. From a safety basis perspective, water solubility could also have significant impact on source term calculations for TA-55, and the corresponding estimated dose to a worker or to a member of the public due to an accidental release of radioactive material. Water solubility of plutonium and uranium compounds can determine the lung clearance rate for inhaled particulates, and this affects the calculation of the committed effective dose equivalent.¹⁻³ Finally, understanding water solubility has nuclear material control and accountability implications, and could affect attractiveness level and termination of safeguards determinations.⁴ The purpose of this report is to document the water solubility of the predominant plutonium and uranium compounds and residues at TA-55.

1.2 Conditions of Criticality Concern

The primary driver of this report is the water solubility of fissionable nuclear materials and the implications for criticality safety. Plutonium/uranium-bearing compounds and residues present in plutonium glovebox processing operations have different solubilities in water. To illustrate the bounding case of a highly soluble plutonium compound, Figure 32 from LA-10860⁵ has been reproduced below in Figure 1-1 with a blue volume vs. density line for 520 g of Pu superimposed. The limiting critical density is 0.0076 kg/L of Pu, and concentrations below this level are of no criticality concern. Above this concentration, conditions for criticality are based upon the volume of water present and the concentration of dissolved plutonium (Figure 1-1). The blue line intersects the water-reflected line at ~17 L, indicating that 520 g of Pu dissolved in 17 L of water (0.031 kg/L Pu) in a spherical configuration will become critical when immersed in a large volume of water that acts as a neutron reflector. For an unreflected spherical solution it takes about 900 g of Pu in 17 L (0.053 kg/L Pu) to reach a critical mass. For comparison, red lines corresponding to various elemental masses of Pu are also shown. These diagrams for Pu-239 are bounding with respect to U-235 for the purposes of criticality safety. The solubility of plutonium and uranium is often determined by a complex combination of conditions, complexation and redox behavior, often leading to low solubility at near-neutral pH.^{1, 6-9} This will be discussed in detail below for various compounds and residues found at TA-55.

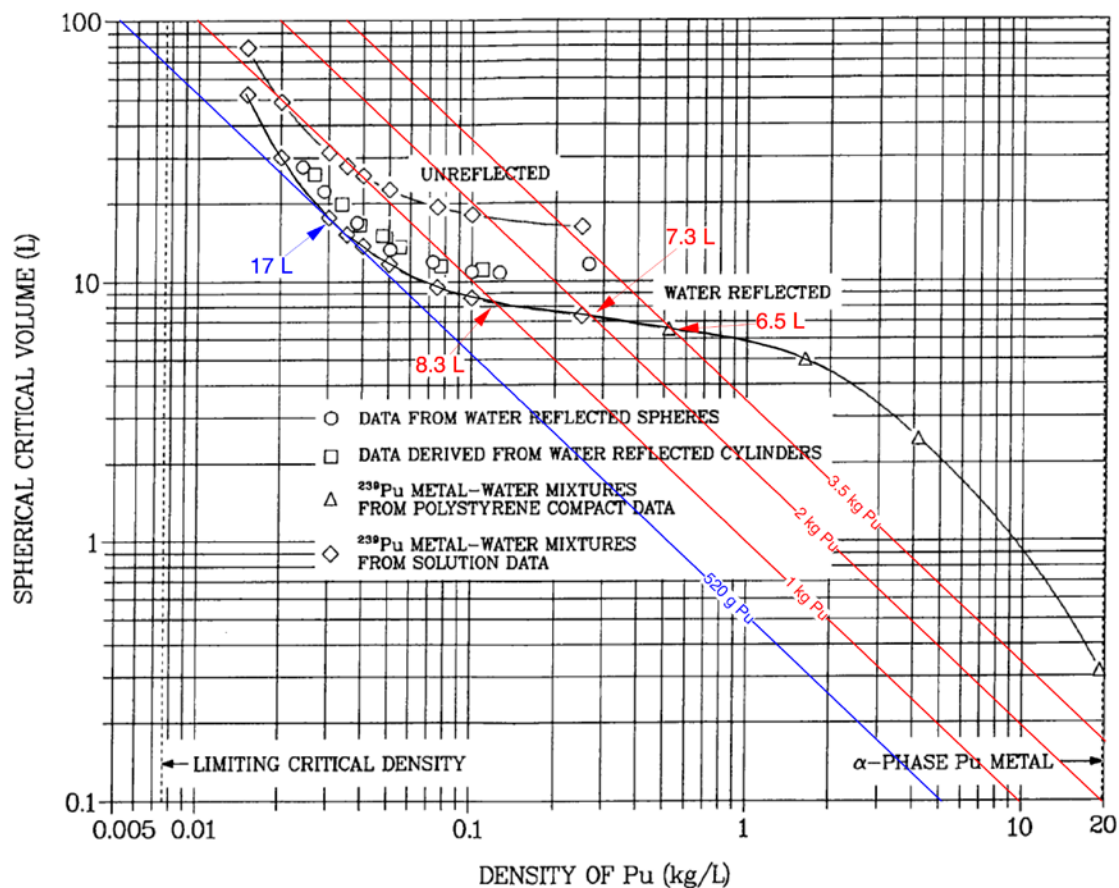


Figure 1-1. Critical volumes of homogeneous water-moderated plutonium spheres. The points suggesting an intermediate curve apply to water-reflected $\text{Pu}(\text{NO}_3)_4$ solution with 1 M HNO_3 and 3.1% ^{240}Pu content of the plutonium (black and white figure and caption reproduced from LA-10860-MS). The blue and red lines show the solution volumes as a function of Pu density (kg/L Pu in solution) for various Pu element masses. The arrows indicate the approximate minimum critical volumes for the water reflected case.

2 Computational Methods

In this report, solution thermodynamic calculations were used to model the water solubility of various solid plutonium residues and compounds relevant to TA-55. Solubility conditions for this discussion refer specifically to the scenario whereby the Pu/U-bearing compounds and dry residues are immersed in water from a fire suppression system. TA-55 fire suppression system water is supplied by Los Alamos County and nothing is added to the PF-4 portion of the fire suppression system water.¹⁰ The fire suppression water is assumed to be pH 7, an E_h of 0.4011 V at a temperature of 25 °C. In the models, water is added in increments to simulate ingress of water into a glovebox. At each volume of water, the equilibrium calculations are performed at constant E_h and temperature, and it is assumed that equilibrium is reached rapidly.

The chemical equilibrium modeling software program Hydra/Medusa¹¹ was used to calculate the solubility and speciation of plutonium under various conditions (e.g., the plutonium speciation was calculated for various relevant combinations of Pu mass, Pu chemical form, water volume added, and matrix constituents). The output from Hydra/Medusa was compared to that obtained using the additional equilibrium modeling software MINEQL+¹² and HySS¹³ in order to validate the results.

The NEA has published a series of books in which they have critically reviewed the thermodynamic equilibrium constants of plutonium and other actinides.¹⁴⁻¹⁵ These served as the source for plutonium solubility, complexation, and redox equilibria used for the calculations. For reference, the constants and their associated equilibrium expressions are shown in Table 2-1. Technical reports and published literature were also used where available to support the solubility estimates.

Table 2-1. Chemical equilibria and equilibrium constants

Species / Compound	Chemical Equilibrium	Equilibrium Constant
Pu^{4+}	$\text{Pu}^{3+} \rightleftharpoons \text{Pu}^{4+} + \text{e}^-$	$\log K^\circ = -17.69^a$
PuO_2^+	$\text{Pu}^{3+} + 2\text{H}_2\text{O} \rightleftharpoons \text{PuO}_2^+ + 4\text{H}^+ + 2\text{e}^-$	$\log K^\circ = -35.15^a$
PuO_2^{2+}	$\text{Pu}^{3+} + 2\text{H}_2\text{O} \rightleftharpoons \text{PuO}_2^{2+} + 4\text{H}^+ + 3\text{e}^-$	$\log K^\circ = -50.97^a$
PuOH^{2+}	$\text{Pu}^{3+} + \text{H}_2\text{O} \rightleftharpoons \text{PuOH}^{2+} + \text{H}^+$	$\log K^\circ = -6.9^b$
$\text{Pu}(\text{OH})_3(\text{cr})$	$\text{Pu}^{3+} + 3\text{H}_2\text{O} \rightleftharpoons \text{Pu}(\text{OH})_3(\text{cr}) + 3\text{H}^+$	$\log K^\circ = -15.8^b$
PuCl^{2+}	$\text{Pu}^{3+} + \text{Cl}^- \rightleftharpoons \text{PuCl}^{2+}$	$\log K^\circ = 0.24^c$
PuCl_2^+	$\text{Pu}^{3+} + 2\text{Cl}^- \rightleftharpoons \text{PuCl}_2^+$	$\log K^\circ = -0.74^c$
$\text{PuCl}_3(\text{cr})$	$\text{Pu}^{3+} + 3\text{Cl}^- \rightleftharpoons \text{PuCl}_3(\text{cr})$	$\log K^\circ = -14.16^a$

Species / Compound	Chemical Equilibrium	Equilibrium Constant
PuOCl(cr)	$\text{Pu}^{3+} + \text{Cl}^- + \text{H}_2\text{O} \rightleftharpoons \text{PuOCl}(\text{cr}) + 2\text{H}^+$	$\log K^\circ = -11.38^{\text{a}}$
PuPO ₄ (s, hyd)	$\text{Pu}^{3+} + \text{PO}_4^{3-} \rightleftharpoons \text{PuPO}_4(\text{s, hyd})$	$\log K^\circ = 24.6^{\text{b}}$
PuOH ³⁺	$\text{Pu}^{4+} + \text{H}_2\text{O} \rightleftharpoons \text{PuOH}^{3+} + \text{H}^+$	$\log K^\circ = 0.6^{\text{b}}$
Pu(OH) ₂ ²⁺	$\text{Pu}^{4+} + 2\text{H}_2\text{O} \rightleftharpoons \text{Pu}(\text{OH})_2^{2+} + 2\text{H}^+$	$\log K^\circ = 0.6^{\text{b}}$
Pu(OH) ₃ ⁺	$\text{Pu}^{4+} + 3\text{H}_2\text{O} \rightleftharpoons \text{Pu}(\text{OH})_3^+ + 3\text{H}^+$	$\log K^\circ = -2.3^{\text{b}}$
Pu(OH) ₄ (aq)	$\text{Pu}^{4+} + 4\text{H}_2\text{O} \rightleftharpoons \text{Pu}(\text{OH})_4(\text{aq}) + 4\text{H}^+$	$\log K^\circ = -8.5^{\text{b}}$
PuO ₂ (am, hyd)	$\text{Pu}^{4+} + 2\text{H}_2\text{O} \rightleftharpoons \text{PuO}_2(\text{am, hyd}) + 4\text{H}^+$	$\log K^\circ = 2.33^{\text{a}}$
PuCl ³⁺	$\text{Pu}^{4+} + \text{Cl}^- \rightleftharpoons \text{PuCl}^{3+}$	$\log K^\circ = 1.8^{\text{b}}$
PuH ₃ PO ₄ ⁴⁺	$\text{Pu}^{4+} + \text{PO}_4^{3-} + 3\text{H}^+ \rightleftharpoons \text{PuH}_3\text{PO}_4^{4+}$	$\log K^\circ = 24.1^{\text{a}}$
Pu(HPO ₄) ₂ (am, hyd)	$\text{Pu}^{4+} + 2\text{PO}_4^{3-} + 2\text{H}^+ \rightleftharpoons \text{Pu}(\text{HPO}_4)_2(\text{am, hyd})$	$\log K^\circ = 55.15^{\text{a}}$
PuO ₂ OH(aq)	$\text{PuO}_2^+ + \text{H}_2\text{O} \rightleftharpoons \text{PuO}_2\text{OH}(\text{aq}) + \text{H}^+$	$\log K^\circ = -9.73^{\text{b}}$
PuO ₂ OH(am)	$\text{PuO}_2^+ + \text{H}_2\text{O} \rightleftharpoons \text{PuO}_2\text{OH}(\text{am}) + \text{H}^+$	$\log K^\circ = -5.0^{\text{b}}$
PuO ₂ OH ⁺	$\text{PuO}_2^{2+} + \text{H}_2\text{O} \rightleftharpoons \text{PuO}_2\text{OH}^+ + \text{H}^+$	$\log K^\circ = -5.5^{\text{b}}$
PuO ₂ (OH) ₂ (aq)	$\text{PuO}_2^{2+} + 2\text{H}_2\text{O} \rightleftharpoons \text{PuO}_2(\text{OH})_2(\text{aq}) + 2\text{H}^+$	$\log K^\circ = -13.2^{\text{b}}$
(PuO ₂) ₂ (OH) ₂ ²⁺	$2\text{PuO}_2^{2+} + 2\text{H}_2\text{O} \rightleftharpoons (\text{PuO}_2)_2(\text{OH})_2^{2+} + 2\text{H}^+$	$\log K^\circ = -7.5^{\text{b}}$
PuO ₂ (OH) ₂ ·H ₂ O(cr)	$\text{PuO}_2^{2+} + 3\text{H}_2\text{O} \rightleftharpoons \text{PuO}_2(\text{OH})_2 \cdot \text{H}_2\text{O}(\text{cr}) + 2\text{H}^+$	$\log K^\circ = -5.5^{\text{b}}$
PuO ₂ Cl ⁺	$\text{PuO}_2^{2+} + \text{Cl}^- \rightleftharpoons \text{PuO}_2\text{Cl}^+$	$\log K^\circ = 0.23^{\text{b}}$
PuO ₂ Cl ₂ (aq)	$\text{PuO}_2^{2+} + 2\text{Cl}^- \rightleftharpoons \text{PuO}_2\text{Cl}_2(\text{aq})$	$\log K^\circ = -1.15^{\text{b}}$
HPO ₄ ²⁻	$\text{H}^+ + \text{PO}_4^{3-} \rightleftharpoons \text{HPO}_4^{2-}$	$\log K^\circ = 12.35^{\text{d}}$
H ₂ PO ₄ ⁻	$2\text{H}^+ + \text{PO}_4^{3-} \rightleftharpoons \text{H}_2\text{PO}_4^-$	$\log K^\circ = 19.562^{\text{a}}$
H ₃ PO ₄ (aq)	$3\text{H}^+ + \text{PO}_4^{3-} \rightleftharpoons \text{H}_3\text{PO}_4(\text{aq})$	$\log K^\circ = 21.702^{\text{a}}$

^aSee Appendix 1. ^bTable 5–2 of ref 15. ^cSection 11.3.1.1 of ref 15. ^dTable 8–2 of ref 15.

3 Results and Discussion

The results of the solubility analysis are described in this section. Sections 3.1 and 3.2 describe the results for plutonium compounds and plutonium residues, respectively. Sections 3.3 and 3.4 describe the results for uranium compounds and uranium residues, respectively. The nuclear material control system at TA-55 relies on Item Description Codes (IDC) to assign a chemical form to each accountable nuclear material item, and the subsections are organized alphabetically by IDC. Individual compound solubility was determined using published solubility data and solution thermodynamic modeling. Residue solubility was estimated using process knowledge, operating procedures and published technical reports to determine their constituent compounds, and then applying the knowledge gained from the compound solubility results to each residue type. The scope of materials considered here includes all compounds and residues at TA-55 as of March 2016 that contain Pu-239 or U-235 where any single item in the facility has more than 500 g of nuclear material. In addition, Section 3.1.3 describes the solubility of plutonium phosphate, even though PuPO_4 is not currently used at TA-55. This section was added to provide a technical basis for using phosphate buffers as part of a criticality safety control set due to the tendency of soluble PuCl_3 to react to precipitate PuPO_4 from aqueous solution. A summary table showing the solubility results is included in Section 3.5 (Table 3-1).

3.1 Plutonium Compounds

3.1.1 Plutonium Chloride (C19)



Figure 3-1. Plutonium Trichloride (C19 and C82)

A photograph of a typical plutonium trichloride salt is shown in Figure 3-1. Trivalent solid PuCl_3 is very soluble in water,⁸ and as it dissolves it hydrolyzes, lowering the pH of resulting solutions. The solubility and complexation behavior of trivalent plutonium often mirrors that of the trivalent lanthanides, which all dissolve to give saturated pH 1–2 solutions of close to 50 wt % lanthanide.¹⁶

Figure 3-2 superimposes a dotted red volume vs. density line for 2,390 g of soluble Pu^{17} on the water-reflected critical density curve (LA-10860 Fig 32.⁵). The solid red line shows the calculated concentration of 2,390 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added water volume. For this quantity of plutonium, the red line crosses the curve at a volume of 7.1 L. The speciation

diagrams in Figure 3-3 (2,390 g Pu) and Figure 3-4 (841 g Pu) indicate that, thermodynamically, $\text{PuCl}_3(\text{s})$ is completely soluble in water. These diagrams also show that the pH drops immediately to ~ 2.3 upon dissolution of 2,390 g Pu and to ~ 2.4 upon dissolution of 841 g Pu. It is noteworthy that the trivalent Pu(III) oxidation state is stable at acidic pH, but will convert to Pu(IV) above pH 6 and precipitate out as a hydroxide in the absence of strong complexants:

The hydrolysis of Pu^{3+} can be studied only with careful control of the plutonium solubility and maintenance of an inert or reducing atmosphere to avoid oxidation to Pu^{4+} , which is increasingly favored as the solution pH is raised.¹⁸

The reason that the PuCl_3 remains in the trivalent oxidation state under the present model results from the observation that, as water is added to such a large quantity of PuCl_3 , the Pu(III) hydrolyzes and lowers the solution pH to a point where Pu(III) is stable (see Figure 3-3 and Figure 3-4). The fact that plutonium becomes insoluble at high pH suggests the possibility of using a hydroxide salt as a criticality safety control inside a glovebox to transform the plutonium from a soluble form to an insoluble form.

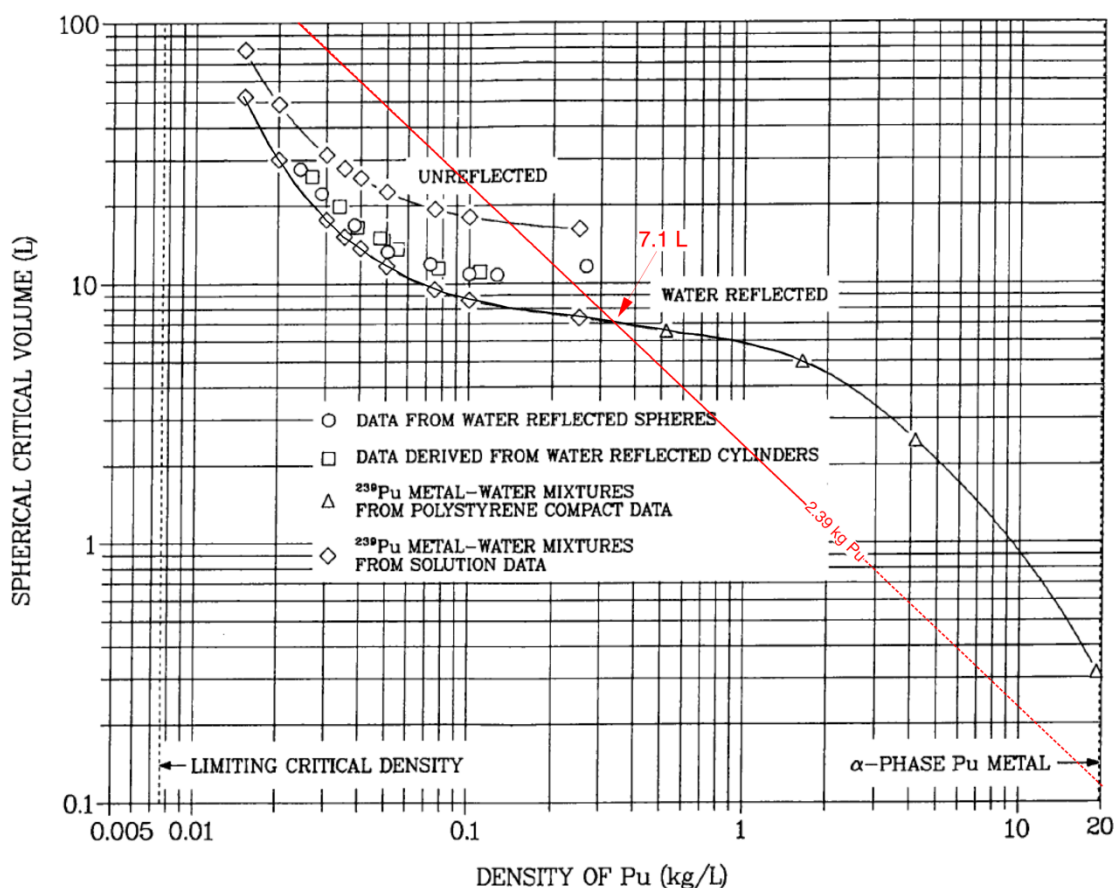


Figure 3-2. Critical volumes of homogeneous water-moderated plutonium spheres (reproduced from LA-10860-MS). The red line plots the quantity of Pu that dissolves for a given volume of water (expressed as kg Pu/L H_2O on the x-axis for a given volume of water on the y-axis).

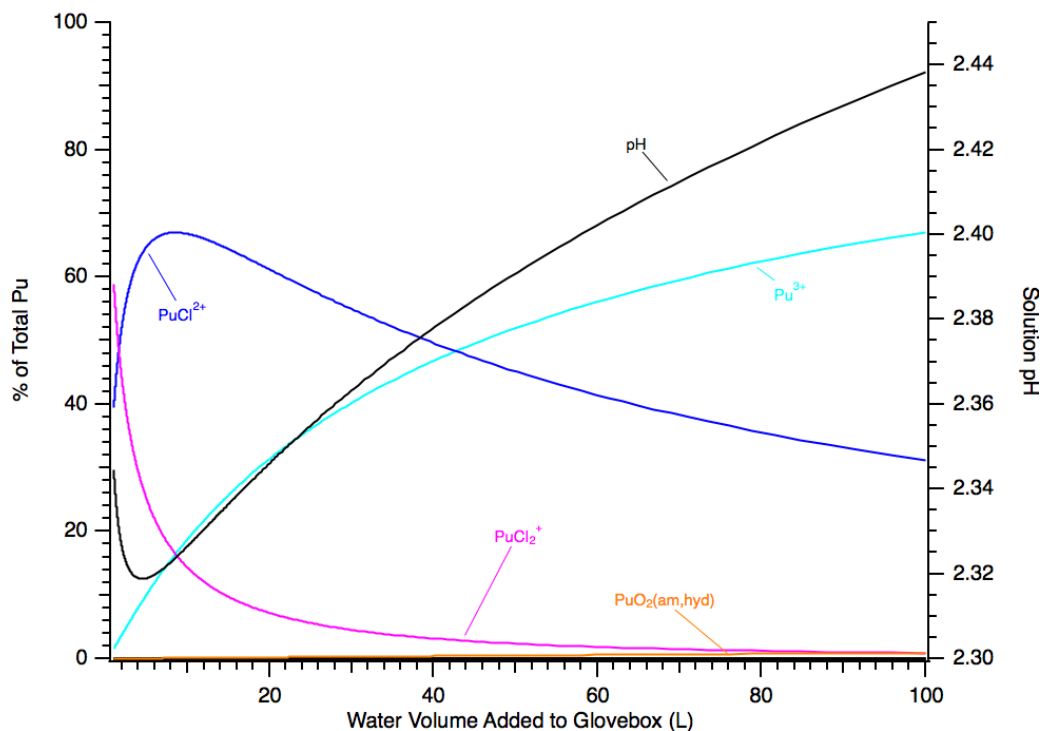


Figure 3-3. Speciation of 2,390 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.

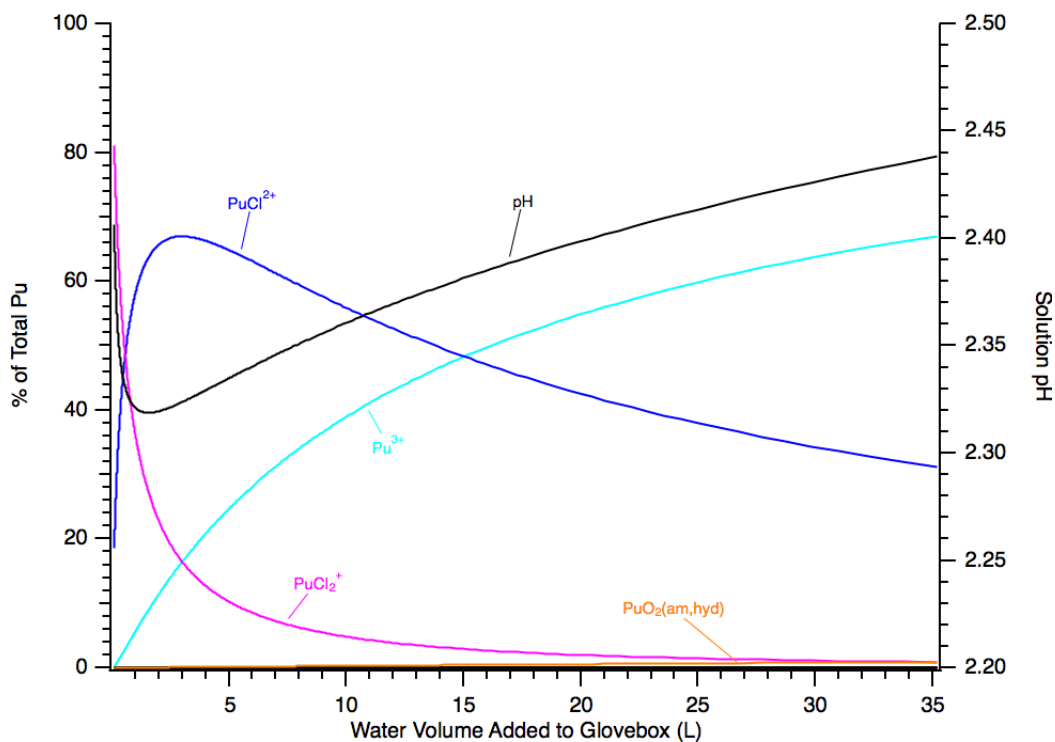


Figure 3-4. Speciation of 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.

3.1.2 Plutonium Dioxide (C21)



Figure 3-5. Plutonium Dioxide (C21).

A photograph of a typical plutonium dioxide compound is shown in Figure 3-5. Plutonium dioxide, $\text{PuO}_2(\text{s})$, has low solubility in water and does not dissolve readily even in strong acid.¹⁹

Figure 3-6 reproduces the water-reflected line from Figure 1-1 (shown as a blue line) and shows the calculated solubility of PuO_2 (am, hyd) (red line).

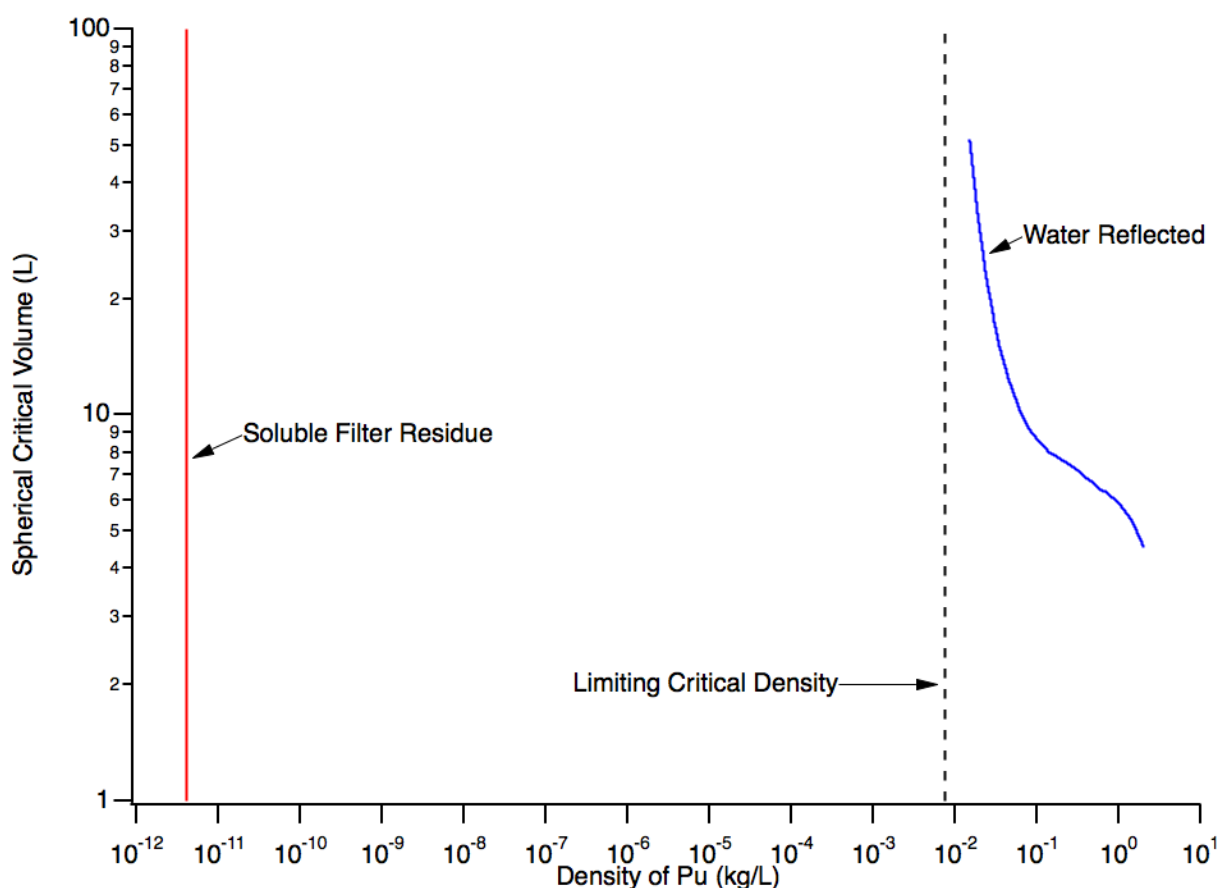


Figure 3-6. Critical volumes of homogeneous water-moderated plutonium spheres (blue line, reproduced from LA-10860-MS). The red line plots the quantity of Pu that

dissolves for a given volume of water (expressed as kg Pu/L H₂O on x-axis for a given volume of water on y-axis).

The speciation plot in Figure 3-7 for 2,450 g Pu as PuO₂(am, hyd) as a function of added water volume confirms that PuO₂ is very insoluble.

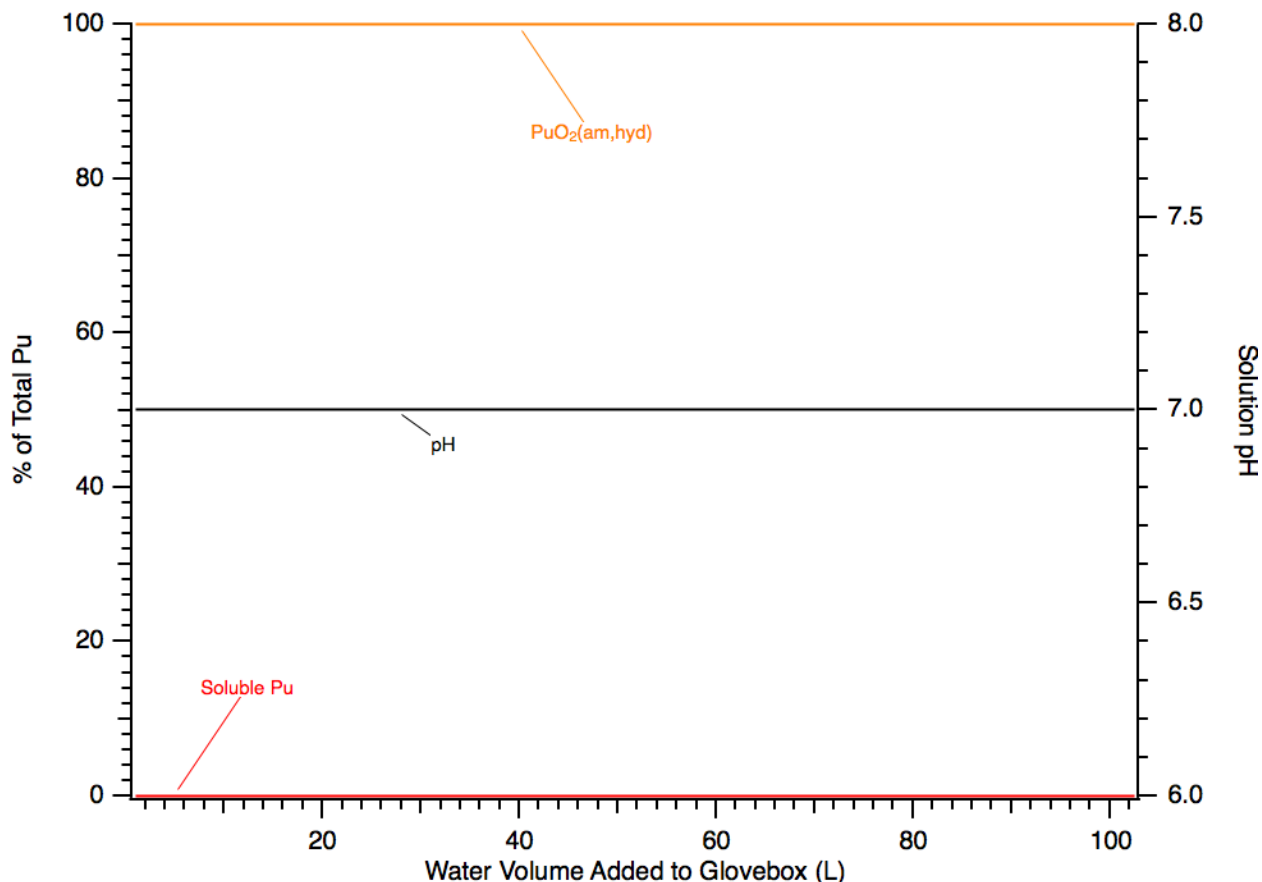


Figure 3-7. Speciation of 2,450 g Pu as PuO₂(am, hyd) as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.

The chemical formula of Pu(IV) hydroxide precipitate is uncertain but expected to be either amorphous hydroxide Pu(OH)₄(am) or hydrous oxide PuO₂·xH₂O(am),^{14, 20-21} referred to here as PuO₂(am, hyd). Consequently, the solubility constant for PuO₂(am, hyd) in Table 2-1 may be used to model the solubility of both plutonium dioxide and Pu(IV) hydroxide precipitates. This is a conservative assumption for PuO₂ (IDC=C21), which may in fact be more crystalline as a result of aging or calcination. Regardless, the references cited here firmly establish that Pu(IV) oxides and hydroxides exhibit negligible solubility in water, and that strongly acidic conditions such as concentrated HNO₃/HF mixtures are required to dissolve PuO₂.⁸

3.1.3 Plutonium Phosphate (C66)

Plutonium phosphate (PuPO₄) is insoluble in water. Figure 3-8 shows three different red volume vs. density lines for a scenario in which 841 g of Pu as PuCl₃(s) is dissolved in water,

superimposed on the water-reflected critical density curve (LA-10860 Fig 32.)⁵ The dotted red line indicates that, as observed in Section 3.1.1, the 841 g of Pu will dissolve. The two red lines illustrate that the Pu solubility can be significantly reduced by adding 0.094 M K_2HPO_4 /0.006 M KH_2PO_4 buffer, and further reduced by adding 0.72 M K_2HPO_4 /0.28 M KH_2PO_4 buffer, resulting in the precipitation of PuPO_4 .

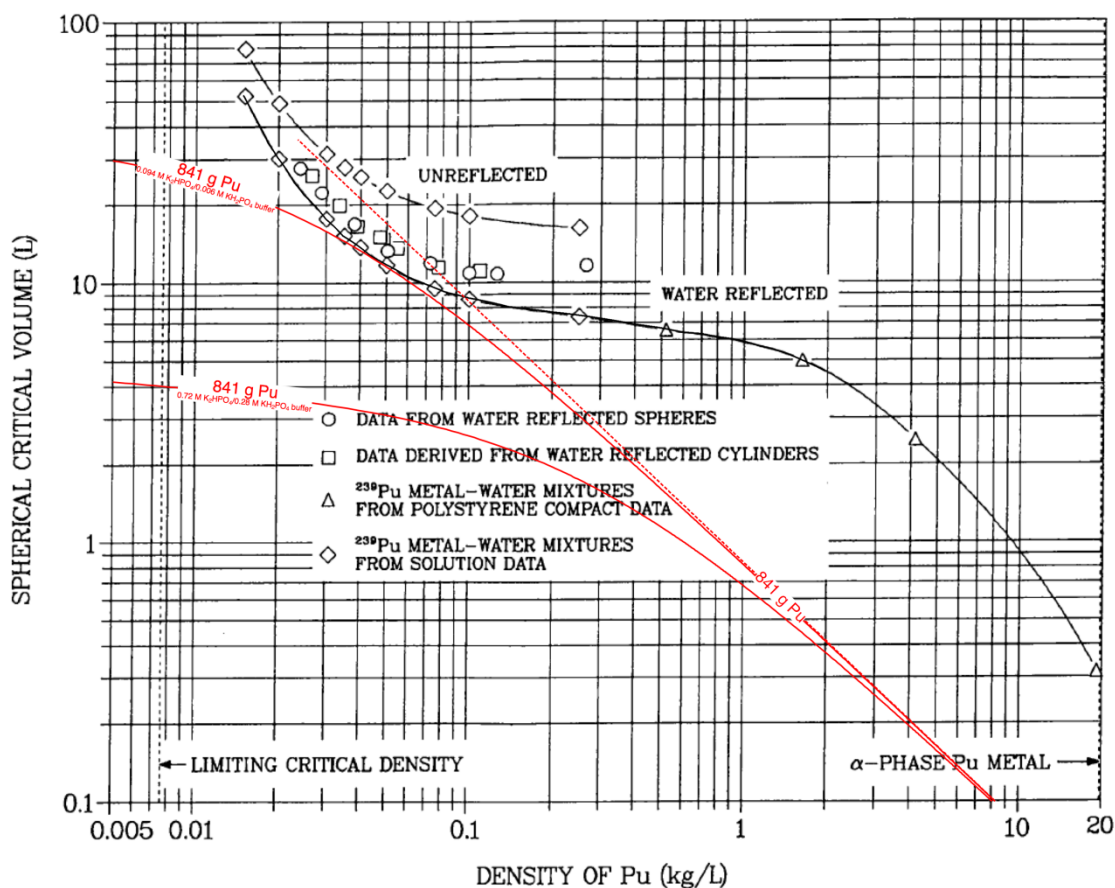


Figure 3-8. Critical volumes of homogeneous water-moderated plutonium spheres (reproduced from LA-10860-MS). The dotted red line shows the quantity of Pu that dissolves for a given volume of water (expressed as kg Pu/L H_2O on the x-axis for a given volume of water on the y-axis). The two red lines illustrate that the Pu solubility can be significantly reduced by adding 0.094 M K_2HPO_4 /0.006 M KH_2PO_4 buffer, and further reduced by adding 0.72 M K_2HPO_4 /0.28 M KH_2PO_4 buffer, resulting in the precipitation of PuPO_4 .

A speciation diagram is illustrated in Figure 3-9 for 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added 0.094 M K_2HPO_4 /0.006 M KH_2PO_4 buffered water volume. The diagram illustrates the effect of precipitation of PuPO_4 . Pu precipitation is even more pronounced when water containing 0.72 M K_2HPO_4 /0.28 M KH_2PO_4 is added to $\text{PuCl}_3(\text{s})$ (Figure 3-10). Thus, if the fire suppression water were assumed to be buffered with a commercially-available phosphate buffer, the solubility of $\text{PuCl}_3(\text{s})$ would be reduced, thus mitigating the risk of a criticality incident. Buffering of firewater with phosphate reagents could be accomplished by placing the chemical agent within

gloveboxes of concern, or buffering the actual firewater (or portion thereof), or using a combination of these approaches.

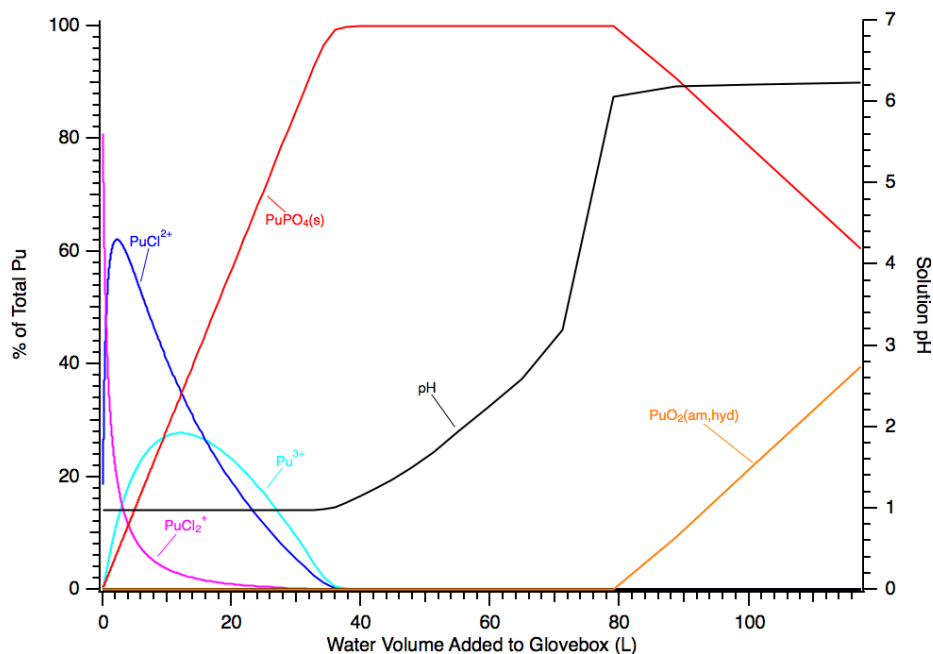


Figure 3-9. Speciation of 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added 0.094 M K_2HPO_4 /0.006 M KH_2PO_4 buffered water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.

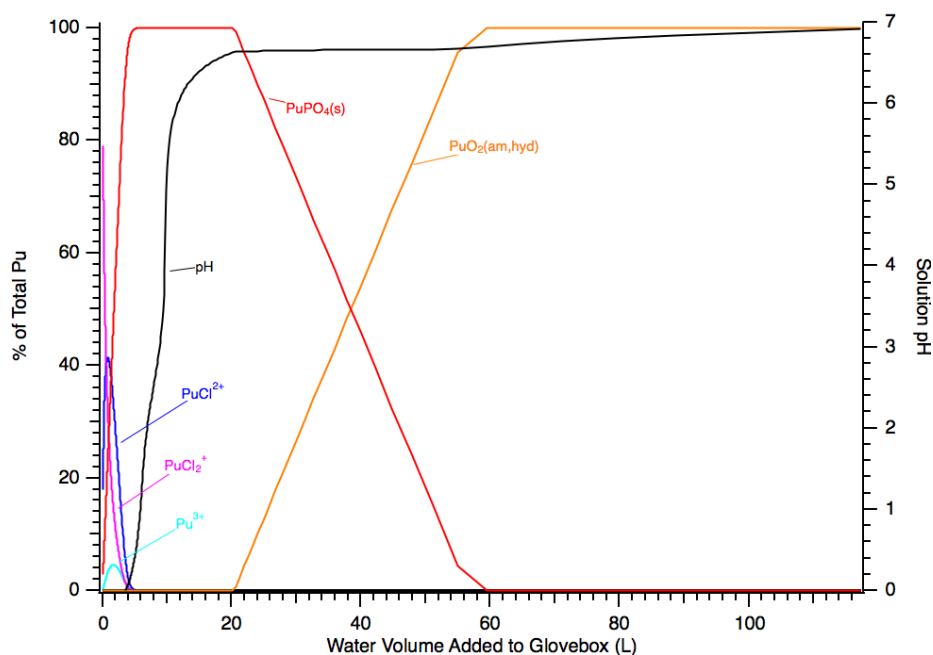


Figure 3-10. Speciation of 841 g Pu as $\text{PuCl}_3(\text{s})$ as a function of added 0.72 M K_2HPO_4 /0.28 M KH_2PO_4 buffered water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.

3.1.4 Plutonium Tetrafluoride (C80)

Plutonium tetrafluoride, $\text{PuF}_4(\text{s})$, has a low solubility in water of 0.1 g Pu / L, and the solubility product constant, $K_{\text{sp}} = 6 \times 10^{-20}$.²²

3.1.5 Plutonium Oxychloride

There are conflicting reports on the solubility of plutonium oxychloride PuOCl in water. Equilibrium calculations suggest that it is quite soluble in water, but it has been reported that PuOCl in electro-refining residues (R65) is insoluble in water (see Section 3.2.6).²³ Figure 3-11 superimposes a dotted red volume vs. density line for 2,390 g of soluble Pu on LA-10860 Fig 32.⁵ The solid red line shows the calculated solubility of 2,390 g Pu as $\text{PuOCl}(\text{s})$ as a function of water volume.

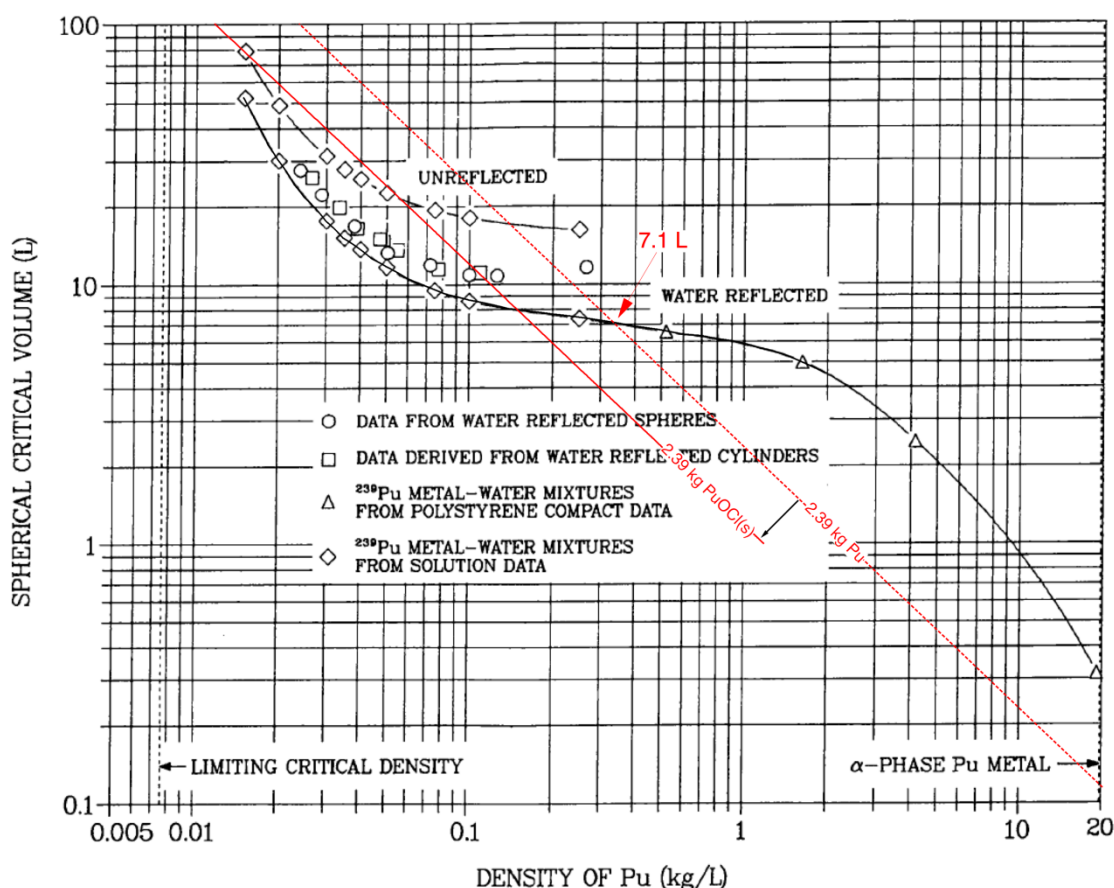


Figure 3-11 Critical volumes of homogeneous water-moderated plutonium spheres (blue line, reproduced from LA-10860-MS). The red line plots the quantity of Pu from PuOCl that dissolves for a given volume of water (expressed as kg Pu/L H_2O on x-axis for a given volume of water on y-axis).

The speciation diagram in Figure 3-12 indicates that, relative to $\text{PuCl}_3(\text{s})$, the addition of water to an equivalent mass of Pu in the form of $\text{PuOCl}(\text{s})$ will lead to less soluble Pu. This appears to be a result of the presence of less chloride which can complex $\text{Pu}(\text{III})$, and not because $\text{PuOCl}(\text{s})$ is less soluble than $\text{PuCl}_3(\text{s})$. This suggests that the case for the solubility of $\text{PuOCl}(\text{s})$ is bounded by the case for $\text{PuCl}_3(\text{s})$. It should be noted that pyrochemical salts generally have additional

salts, such as CaCl_2 cover salt, and additional dissolved chloride ion would tend to make the PuOCl even more soluble.

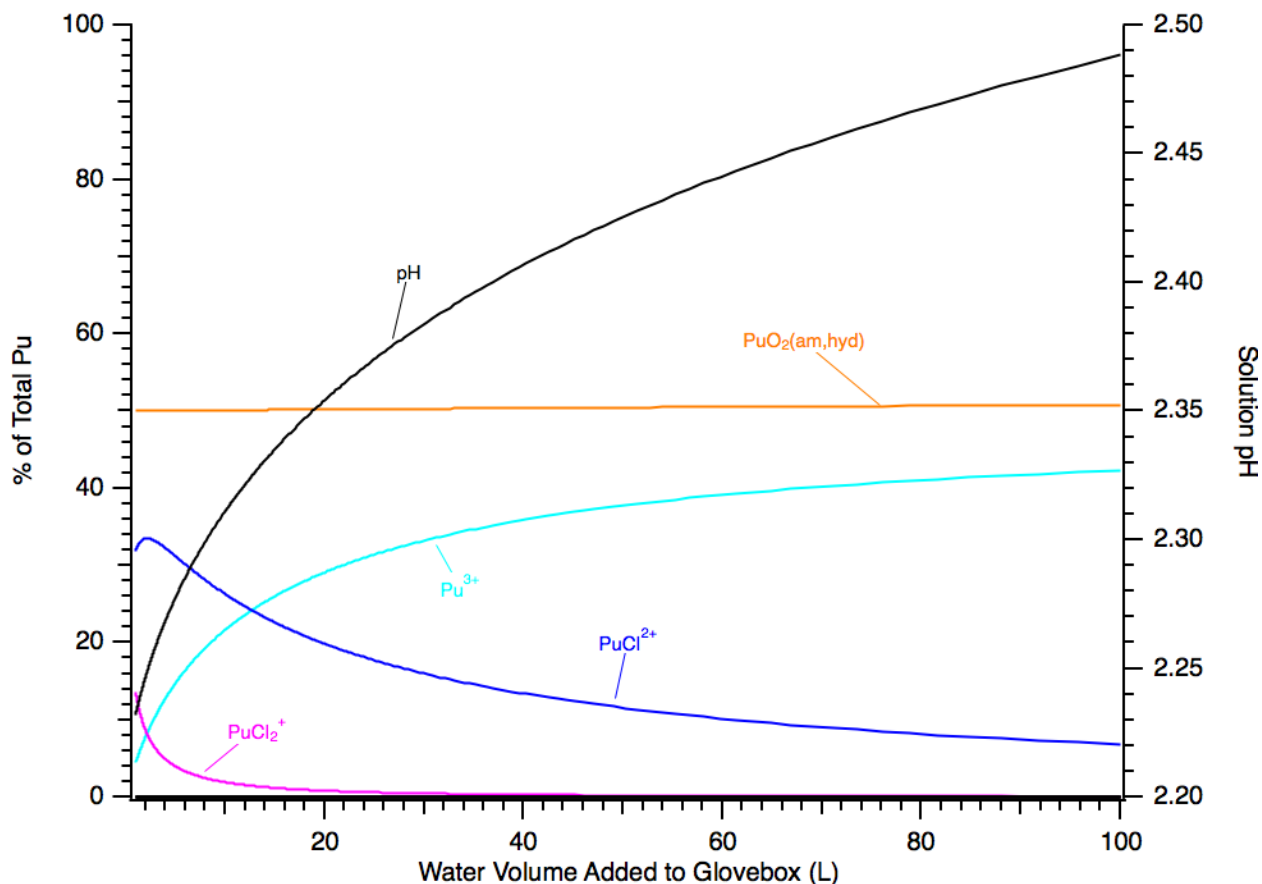


Figure 3-12 Speciation of 2,390 g Pu as $\text{PuOCl}(\text{s})$ as a function of added water volume. Colored lines for individual Pu solid and solution species are plotted against the left y-axis. The black solution pH line is plotted against the right y-axis.

3.2 Plutonium Residues

3.2.1 Plutonium Calcium Salt (R09)

The chemical form and solubility of this residue is uncertain. The DOR process generates calcium chloride-bearing salt residues, and it is possible that this residue will have solubility behavior analogous to that of DOR salts (R42). Alternatively, some MSE salts have a CaCl_2 cover salt,²⁴ so it is possible that this residue will have solubility behavior analogous to that of MSE salts (R83). Further information about the nature of this residue may be ascertained by examining historical process information or by experiment.

3.2.2 Plutonium Filter Residue (R26)



Figure 3-13. Plutonium filter residue (dissolution heel) from aqueous nitrate dissolution process. This is the material that remains undissolved and is subsequently collected by filtration after heating a plutonium residue in strong nitric acid solution.

A photograph of a typical plutonium filter residue is shown in Figure 3-13. This material is the residue that remains undissolved when a process residue is digested in hot concentrated hydrochloric²⁵ or nitric acid²⁶, and therefore it will have negligible solubility in water. The plutonium in these refractory residues is expected to be in the chemical form of Pu(IV) oxides and/or hydroxides,^{8, 27-28} referred to here as PuO₂(am, hyd). Given the expectation that the primary form of plutonium in this residue is PuO₂(am, hyd), the calculations in Section 3.1.2 confirm the expectation that R26 plutonium filter residues have negligible solubility in water.

3.2.3 Plutonium Hydroxide Precipitate (R41)

Sodium or potassium hydroxide is commonly added to plutonium-bearing solutions to precipitate the plutonium. The chemical composition of this residue is Pu(IV) hydroxide,²⁹⁻³⁰ referred to here as PuO₂(am, hyd) as discussed in Section 3.1.2. Therefore, these R41 plutonium hydroxide precipitates will have negligible solubility in water.

3.2.4 Plutonium Direct Oxide Reduction (DOR) Salt (R42)



Figure 3-14. Plutonium Direct Oxide Reduction (DOR) Salt (R42). The plutonium metal button product is pictured on top of the calcium salt cake.

In the direct oxide reduction (DOR) process, plutonium dioxide is reduced by calcium metal in molten CaCl_2 solvent to form plutonium metal and calcium oxide.³¹⁻³³ A typical plutonium DOR salt is illustrated in Figure 3-14. These salts are largely CaCl_2 but may contain CaO , finely divided Ca metal and Pu shot which may subsequently be oxidized to PuO_2 .³⁴ The Pu shot and PuO_2 in DOR residues will have negligible solubility in water. In addition, both CaO and Pu metal form basic solutions when exposed to water, which would lead to $\text{PuO}_2(\text{s})$ formation. Furthermore, experimental data indicates that exposure of oxidized DOR salt to water yields a solution phase containing dissolved CaCl_2 with negligible Pu content ($< 0.0001 \text{ kg Pu/L}$), and a solid PuO_2 phase.³⁴

3.2.5 Plutonium Incinerator Ash (R47)

Plutonium incinerator ash is primarily PuO_2 and therefore they will have negligible solubility in water,^{8, 29, 35} as evidenced by the following quote:

Ash from the incineration of these materials has proven to be one of the more difficult matrices from which to solubilize plutonium.³⁵

3.2.6 Plutonium Electrorefining (ER) Salt (R65)



Figure 3-15. Plutonium Electrorefining (ER) Salt (R65).

In the electrorefining (ER) process, impure plutonium metal is electrochemically oxidized to PuCl_3 in a molten NaCl/KCl solvent, and is then reduced back to purified Pu metal after undergoing electrochemical transport.³⁶⁻³⁷ Approximately 7% of the starting Pu remains in the salt phase as PuCl_3 or Pu metal shot.³⁸ A typical ER salt is illustrated in Figure 3-15. Because ER salts may contain PuCl_3 , they should be considered as potentially water-soluble.

There is a portion of the TA-55 plutonium ER salt residues that have been oxygen-sparged or stabilized by calcination. These R65 items contain insoluble PuOCl and PuO_2 ²³ and are identified by the addition of "OX" in the item identification name (e.g., "XBSOX..."). Experimental data indicate that these items containing solid PuOCl and/or PuO_2 have negligible solubility in water.²³ This is contrary to the relatively high water solubility of PuOCl noted in Section 3.1.5, and this suggests the possibility that the equilibrium constants used to calculate the solubility of PuOCl do not fully describe the observed chemistry in these residues.

3.2.7 Plutonium Salt (R71)

The chemical form and solubility of this residue has not yet been analyzed. It will be analyzed on a case-by-case basis or determined experimentally.

3.2.8 Plutonium Silica (R73)

The chemical form and solubility of this residue has not yet been analyzed. It will be analyzed on a case-by-case basis or determined experimentally.

3.2.9 Plutonium Sweepings/Screenings (R78)

The solubility of sweepings/screenings could be very process-dependent. It will be analyzed on a case-by-case basis or determined experimentally.

3.2.10 Plutonium Molten Salt Extraction (MSE) Salt (R83)



Figure 3-16. Plutonium Molten Salt Extraction (MSE) Salt (R83).

In the molten salt extraction (MSE) process, plutonium metal with high americium content is reacted with MgCl_2 oxidant in molten NaCl/KCl solvent.³⁹⁻⁴⁰ The MgCl_2 oxidizes the americium metal to form AmCl_3 , which then separates from the purified plutonium metal. However, some plutonium metal is also oxidized to PuCl_3 and settles in the MSE salt. A typical MSE salt is illustrated in Figure 3-16. Because plutonium MSE salts may contain PuCl_3 , they should be considered as potentially water-soluble. Oxygen-sparged MSE salts contain primarily insoluble PuO_2 and PuOCl .⁴¹

3.3 Uranium Compounds

3.3.1 Uranium Carbide (C13)

There are three uranium carbide phases: UC, UC₂, and U₂C₃.⁴² All three phases will react with water by slowly disintegrating to give insoluble U(IV) hydrous oxides (UO₂·xH₂O) and unreacted solid U carbide.⁴³⁻⁴⁶ Hydrogen and a variety of hydrocarbons are also produced, principally methane and ethane for UC and UC₂, respectively. Consequently, negligible soluble uranium would result from contact of TA-55 uranium carbide compounds with water.

3.3.2 Uranium Dioxide (C21)

Uranium dioxide, UO₂(s), has low solubility in water.⁴⁷⁻⁴⁹

3.3.3 Uranium Nitrate (C52)

Uranium(VI) nitrate, UO₂(NO₃)₂·xH₂O(s), is very soluble in water.⁴⁹⁻⁵⁰

3.3.4 Uranium U₃O₈ (C88)

U₃O₈(s), has low solubility in water.⁵¹

3.3.5 Uranium Uranates

Uranates have low solubility in water.⁵² Uranate precipitates are formed when the pH of a uranium solution is raised above 6.5 by adding hydroxide (e.g., NaOH, KOH, NH₄OH). The chemical composition of uranates varies, but is approximately M₂U₂O₇ (where M is the cation of the base used in the precipitation, e.g., Na⁺).

3.4 Uranium Residues

3.4.1 Uranium Filter Residue (R26)

These uranium filter residues are from an electrolytic decontamination process.⁵³ The residue is generated by adding hydroxide to a uranium containing solution until the uranium precipitates out. Consequently, these uranium residues will be in the form of uranates (section 3.3.5) and will be insoluble in water.

3.5 Summary

The summary of water solubility results for plutonium and uranium compounds and residues at TA-55 are listed in Table 3-1. Where quantitative solubility values could be calculated, an estimated range of solubility in g/L has been provided in the table. Where only qualitative solubility information was available, this has been indicated in the table using the designations: i=insoluble, s=soluble. Table 3-1 also includes a column with the section in this report that includes discussion, calculations, and specific references.

Table 3-1. Summary of water solubility results

IDC Code	IDC Code Description	Chemical Form	Total # of Items ^a	# of items >500 g ^a	Water Solubility	Section in this Report
Plutonium Compounds						
C19, C82	Trichloride	PuCl ₃	9	2	> 100 g/L	3.1.1
C21	Dioxide	PuO ₂	2,182	1,020	< 1 g/L	3.1.2
C66	Phosphate	PuPO ₄	0	0	< 1 g/L	3.1.3
C80	Tetrafluoride	PuF ₄	30	2	< 1 g/L	3.1.4
NA	Oxychloride	PuOCl	NA	NA	b	3.1.5
Plutonium Residues						
R09	Calcium Salt	b	1	1	b	3.2.1
R26	Filter Residue	PuO ₂ , Pu(OH) ₄	173	70	< 1 g/L	3.2.2
R41	Hydroxide Precipitate	Pu(OH) ₄	18	1	< 1 g/L	3.2.3
R42	Direct Oxide Reduction (DOR) Salt	PuO ₂ , Pu metal	66	24	< 1 g/L	3.2.4
R47	Incinerator Ash	PuO ₂ , Pu _x O _y	71	7	< 1 g/L	3.2.5
R65	Electrorefining (ER) Salt	PuCl ₃ , PuOCl ^c , Pu metal	508	183	b	3.2.6
R71	Salt	b	86	13	b	3.2.7
R73	Silica	b	16	6	b	3.2.8
R78	Sweepings/Screenings	b	152	10	b	3.2.9
R83	Molten Salt Extraction (MSE) Salt	PuCl ₃ , Pu metal	246	42	> 100 g/L	3.2.10
Uranium Compounds						
C13	Carbide	UC, UC ₂ , U ₂ C ₃	9	5	U(IV) solids	3.3.1
C21	Dioxide	UO ₂	401	112	i	3.3.2
C52	Nitrate	UO ₂ (NO ₃) ₂	2	2	s	3.3.3
C88	U ₃ O ₈	U ₃ O ₈	186	122	i	3.3.4
NA	Uranates	M _x U _y O _z (e.g., Na ₂ U ₂ O ₇)	NA	NA	i	3.3.5
Uranium Residues						
R26	Filter Residue	M _x U _y O _z (e.g., Na ₂ U ₂ O ₇)	45	2	< 1 g/L	3.4.1

^aThe number of items were determined from a LANMAS report performed in March, 2016 for all TA-55 material balance areas where a single item contained >500 g nuclear material (>1 g of plutonium (81-100% Pu-239) or >1 g uranium (0.7-94% U-235))

^bThe chemical makeup and water solubility are uncertain due to conflicting reports, insufficient process knowledge or process-dependent composition.

^cSome ER and MSE salts have been O₂-sparged,^{23, 41} these will contain a mix of PuO₂ and PuOCl.

4 Conclusions

The analyses in this document lead to the conclusion that the following materials are not appreciably soluble in water: plutonium dioxide (IDC=C21), plutonium phosphate (IDC=C66), plutonium tetrafluoride (IDC=C80), plutonium filter residue (IDC=R26), plutonium hydroxide precipitate (IDC=R41), plutonium DOR salt (IDC=R42), plutonium incinerator ash (IDC=R47), uranium carbide (IDC=C13), uranium dioxide (IDC=C21), U_3O_8 (IDC=C88), and uranium filter residue (IDC=R26). The analyses also indicate that the following compounds are soluble in water: plutonium chloride (IDC=C19) and uranium nitrate (IDC=C52). Equilibrium calculations suggest that $PuOCl$ is water soluble, but some plutonium processing reports indicate that it is insoluble when present in electrorefining residues (R65). Plutonium molten salt extraction residues (IDC=R83) contain significant quantities of $PuCl_3$, and are expected to be soluble in water. The solubility of the following plutonium residues is indeterminate due to conflicting reports, insufficient process knowledge or process-dependent composition: calcium salt (IDC=R09), electrorefining salt (IDC=R65), salt (IDC=R71), silica (IDC=R73) and sweepings/screenings (IDC=R78). Solution thermodynamic modeling also indicates that fire suppression water buffered with a commercially-available phosphate buffer would significantly reduce the solubility of $PuCl_3$ by the precipitation of $PuPO_4$. Future solubility experiments on actual residues, particularly ER and MSE salts, could indicate that these residues are not soluble despite the fact that they contain soluble compounds such as $PuCl_3$ or $PuOCl$.

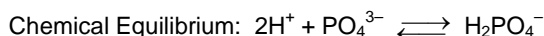
5 References

- (1) *Good Practices for Occupational Radiological Protection in Plutonium Facilities*; DOE-STD-1128-2013; 2013.
- (2) *Guide of Good Practices for Occupational Radiological Protection in Uranium Facilities*; DOE-STD-1136-2009; 2009.
- (3) Smith, P. H.; Jordan, H.; Hoffman, J. A.; Eller, P. G.; Balkey, S. *Health Phys.* **2007**, 92, S87-S97.
- (4) *Nuclear Material Control and Accountability*; DOE M 470.4-6; 2007.
- (5) Paxton, H. C.; Pruvost, N. L. *Critical Dimensions of Systems Containing ^{235}U , ^{239}Pu , and ^{233}U* ; LA-10860-MS; 1987.
- (6) Wick, O. J. *Plutonium Handbook—A Guide to the Technology*; 1967; Vol. Vol 1 (section 2) & Vol 2 (section 5).
- (7) Katz, J. J.; Seaborg, G. T.; Morss, L. R., *The Chemistry of the Actinide Elements*. 2 ed.; Chapman and Hall: New York, 1986; Vol. 1.
- (8) Christensen, E. L.; Maraman, W. J. *Plutonium Processing at the Los Alamos Scientific Laboratory*; LA-3542; Los Alamos Scientific Laboratory: 1969.
- (9) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 813-1264.
- (10) *TA-55 Fire Protection (FP) System Design Description*; SDD-TA55-FP-018; 8/27/14.
- (11) Puigdomenech, I.; Colas, E.; Grive, M.; Campos, I.; Garcia, D. *Materials Research Society Symposium Proceedings* **2014**, 1665, 111-116.
- (12) Schecher, W. D.; McAvoy, D. C. *MINEQL+: A chemical equilibrium modeling system*, Version 4.6 for Windows; Environmental Research Software: Hallowell, ME, 2003.
- (13) Gans, P. *HySS—Hyperquad Simulation and Speciation*, 2006.
- (14) Lemire, R. J.; Fuger, J.; Nitsche, H.; Potter, P.; Rand, M. H.; Rydberg, J.; Spahiu, K.; Sullivan, J. C.; Ullman, W. J.; Vitorge, P.; Wanner, H. *Chemical Thermodynamics of Neptunium and Plutonium*; Elsevier: Amsterdam, 2001; Vol. 4.
- (15) Guillaumont, R.; Fanghänel, T.; Fuger, J.; Grenthe, I.; Neck, V.; Palmer, D. A.; Rand, M. H. *Update on the Chemical Thermodynamics of Uranium, Neptunium, Plutonium, Americium and Technetium*; Elsevier: Amsterdam, 2003; Vol. 5.
- (16) Mioduski, T.; Guminski, C.; Zeng, D. *J. Phys. Chem. Ref. Data* **2008**, 37, 1765-1853.
- (17) As of March 2016 the largest individual residue item at TA-55 that is expected to be composed of PuCl_3 has an element mass of 2,390 g Pu-239.
- (18) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, p 1147.
- (19) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 1048-1049.
- (20) Knopp, R.; Neck, V.; Kim, J. I. *Radiochimica Acta* **1999**, 86, 101-108.

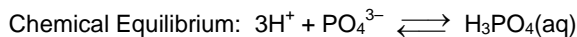
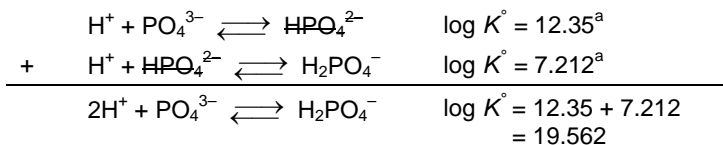
- (21) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 1149-1150.
- (22) Griffo, J. S.; Brown, W. B.; Lonadier, F. D. *Solubility of Plutonium Compounds*; MLM-1191; 1964.
- (23) Garcia, E.; Griego, W. J.; Dole, V. R. *Treating Pyrochemical Salt Residues to Produce Plutonium Dioxide or Plutonium Oxychloride, and Preparing Plutonium Trichloride using Ammonium Chloride*; LA-14124; Los Alamos National Laboratory: 2004.
- (24) Owens, S. D. *Oxidation Studies for Conversion of Plutonium/Americium Chlorides Resulting From In-Situ Chlorination*; LA-13813-T; Los Alamos National Laboratory: 2001.
- (25) *Chloride Extraction Line (CXL) MBA 742*; TA55-PMFD-01039, R2; Los Alamos National Laboratory.
- (26) *Cascade Dissolver (ED) MBA 743*; TA55-PMFD-01031, R0-EXT1; Los Alamos National Laboratory.
- (27) Robinson, M. A.; Kinker, M. B.; Wieneke, R. E. *Modeling Of Plutonium Recovery And Discard Processes For The Purpose Of Selecting Optimum (Minimum Waste, Cost, & Dose) Residue Dispositions*; LA-UR-01-2149; Los Alamos National Laboratory: 2001.
- (28) Robinson, M. A. *Analysis of Plutonium Processing Systems as a Basis for Selecting Dispositions for Actinide-bearing Process Residues That Minimize Negative Quantifiable Consequences Including Proliferation Risks, Radioactive Waste Generation, Personnel Exposure to Ionizing Radiation, and Costs*; LA-UR-03-2233; Los Alamos National Laboratory: 2003.
- (29) Christensen, D. C.; Bowersox, D. F.; McKerley, B. J.; Nance, R. L. *Wastes from Plutonium Conversion and Scrap Recovery Operations*; LA-11069-MS; 1988.
- (30) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, p 838.
- (31) Clark, D. L.; Jarvinen, G.; Kowalczyk, C.; Rubin, J.; Stroud, M. A. *Actinide Research Quarterly* **3rd Quarter 2008**, 10-11.
- (32) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 866-869.
- (33) Mullins, L. J.; Christensen, D. C.; Babcock, B. R. *Fused Salt Processing of Impure Plutonium Dioxide to High-Purity Plutonium Metal*; LA-9154-MS; Los Alamos National Laboratory: 1982.
- (34) Dole, V. R.; Garcia, E. *Aqueous Dissolution of Oxidized Calcium Chloride DOR Residues*; LA-UR-97-1566; Los Alamos National Laboratory: 1997.
- (35) Blum, T. W.; Behrens, R. G.; Salazar, V. J.; Nystrom, P. K. *A Small-Scale Study on the Dissolution and Anion-Exchange Recovery of Plutonium from Rocky Flats Plant Incinerator Ash*; LA-11747; Los Alamos National Laboratory: 1989.
- (36) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 870-872.
- (37) Clark, D. L.; Jarvinen, G.; Kowalczyk, C.; Rubin, J.; Stroud, M. A. *Actinide Research Quarterly* **3rd Quarter 2008**, 13.
- (38) Christensen, D. C.; Mullins, L. J. *ACS Symposium Series* **1983**, 216, 409-31.
- (39) Avens, L. R.; Clifton, D. G.; Vigil, A. R. *Actinide Recovery from Pyrochemical Residues*; LA-10281-MS; Los Alamos National Laboratory: 1985.
- (40) Clark, D. L.; Hecker, S. S.; Jarvinen, G. D.; Neu, M. P. In *The Chemistry of the Actinide and Transactinide Elements*; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 869-870.

- (41) Garcia, E.; Griego, W. J.; Owens, S. D.; Thorn, C. W.; Vigil, R. A. *Oxygen Sparging of Residue Salts*; LA-UR-93-697; Los Alamos National Laboratory: 1993.
- (42) Grenthe, I.; Drozdzyński, J.; Fujino, T.; Buck, E. C.; Albrecht-Schmitt, T. E.; Wolf, S. F. In *The Chemistry of the Actinide and Transactinide Elements*; 3rd ed.; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 399-405.
- (43) Kempter, C. P. *J. Less-Common Met.* **1962**, *4*, 419-25.
- (44) Bradley, M. J.; Ferris, L. M. *Inorg. Chem.* **1964**, *3*, 189-95.
- (45) Bradley, M. J.; Ferris, L. M. *Inorg. Chem.* **1964**, *3*, 730-4.
- (46) Bradley, M. J.; Ferris, L. M. *Inorg. Chem.* **1962**, *1*, 683-7.
- (47) Grenthe, I.; Drozdzyński, J.; Fujino, T.; Buck, E. C.; Albrecht-Schmitt, T. E.; Wolf, S. F. In *The Chemistry of the Actinide and Transactinide Elements*; 3rd ed.; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, p 257.
- (48) Grenthe, I.; Fuger, J.; Konings, R. J. M.; Lemire, R. J.; Muller, A. B.; Nguyen-Trung, C.; Wanner, H. *Chemical Thermodynamics of Uranium*; North-Holland: Amsterdam, 1992; Vol. 1, p. 120.
- (49) Haynes, W. M.; Bruno, T. J.; Lide, D. R., *CRC Handbook of Chemistry and Physics*. CRC Press: Boca Raton, FL, 2016; p 4-97.
- (50) Grenthe, I.; Drozdzyński, J.; Fujino, T.; Buck, E. C.; Albrecht-Schmitt, T. E.; Wolf, S. F. In *The Chemistry of the Actinide and Transactinide Elements*; 3rd ed.; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, pp 359-364.
- (51) Hala, J.; Miyamoto, H. *J. Phys. Chem. Ref. Data* **2007**, *36*, 1417-1736.
- (52) Grenthe, I.; Drozdzyński, J.; Fujino, T.; Buck, E. C.; Albrecht-Schmitt, T. E.; Wolf, S. F. In *The Chemistry of the Actinide and Transactinide Elements*; 3rd ed.; Morss, L. R.; Edelstein, N. M.; Fuger, J.; Katz, J. J., Eds.; Springer: Dordrecht, Netherlands, 2006; Vol. 2, p 313.
- (53) *Operation of the Uranium Electrolytic Decontamination System*; NMT15-WI-143, R1; Los Alamos National Laboratory.

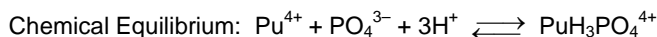
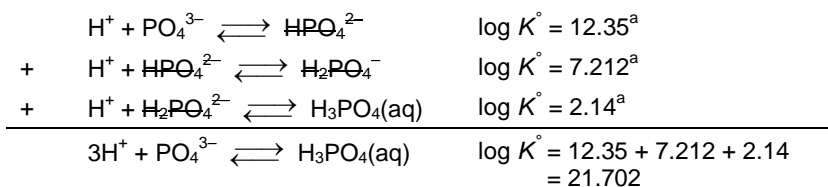
6 Appendix 1. Derivation of Equilibrium Constants



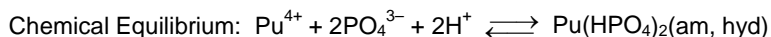
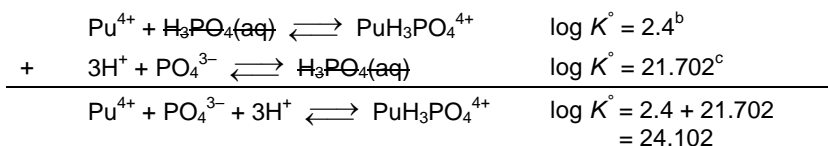
Derivation:



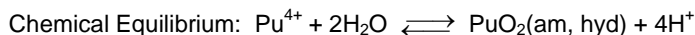
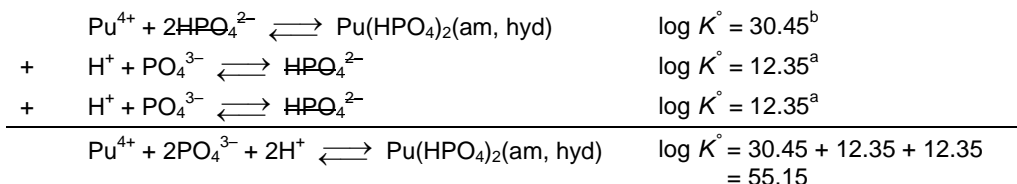
Derivation:



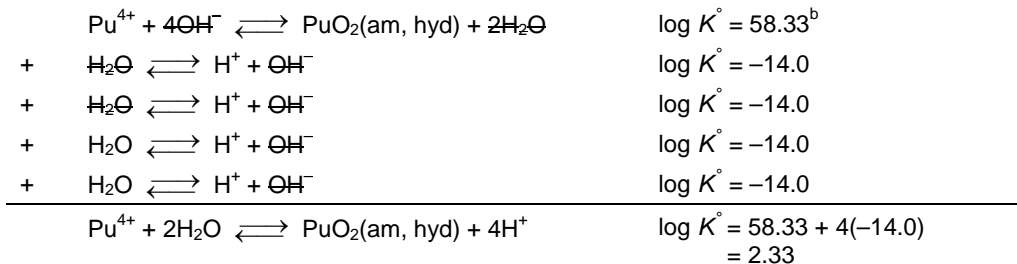
Derivation:



Derivation:



Derivation:





Derivation:

$$\Delta G^\circ = \Delta_f G^\circ(\text{PuOCl}(\text{cr})) + 2\Delta_f G^\circ(\text{H}^+) - \Delta_f G^\circ(\text{Pu}^{3+}) - \Delta_f G^\circ(\text{Cl}^-) - \Delta_f G^\circ(\text{H}_2\text{O})$$

$$\Delta_f G^\circ(\text{PuOCl}(\text{cr})) = -882.409 \text{ kJ/mol}^{\text{d}}$$

$$\Delta_f G^\circ(\text{H}^+) = 0.000 \text{ kJ/mol}^{\text{e}}$$

$$\Delta_f G^\circ(\text{Pu}^{3+}) = -578.984 \text{ kJ/mol}^{\text{d}}$$

$$\Delta_f G^\circ(\text{Cl}^-) = -131.217 \text{ kJ/mol}^{\text{e}}$$

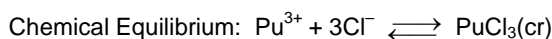
$$\Delta_f G^\circ(\text{H}_2\text{O}) = -237.140 \text{ kJ/mol}^{\text{e}}$$

Therefore:

$$\begin{aligned}\Delta G^\circ &= -882.409 + 2(0.000) - (-578.984) - (-131.217) - (-237.140) \text{ kJ/mol} \\ &= 64.932 \text{ kJ/mol}\end{aligned}$$

$$\ln K = -\frac{\Delta G^\circ}{RT} = -\frac{(64.932 \text{ kJ/mol})(1000 \text{ J/kJ})}{(8.314510 \text{ J/K}\cdot\text{mol})(298.15 \text{ K})} = -26.1931244$$

$$\log K = \log (e^{\ln K}) = \log (e^{-26.1931244}) = -11.38$$



Derivation:

$$\Delta G^\circ = \Delta_f G^\circ(\text{PuCl}_3(\text{cr})) - \Delta_f G^\circ(\text{Pu}^{3+}) - 3\Delta_f G^\circ(\text{Cl}^-)$$

$$\Delta_f G^\circ(\text{PuCl}_3(\text{cr})) = -891.806 \text{ kJ/mol}^{\text{d}}$$

$$\Delta_f G^\circ(\text{Pu}^{3+}) = -578.984 \text{ kJ/mol}^{\text{d}}$$

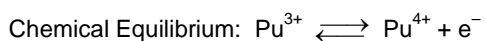
$$\Delta_f G^\circ(\text{Cl}^-) = -131.217 \text{ kJ/mol}^{\text{e}}$$

Therefore:

$$\begin{aligned}\Delta G^\circ &= -891.806 - (-578.984) - 3(-131.217) \text{ kJ/mol} \\ &= 80.829 \text{ kJ/mol}\end{aligned}$$

$$\ln K = -\frac{\Delta G^\circ}{RT} = -\frac{(80.829 \text{ kJ/mol})(1000 \text{ J/kJ})}{(8.314510 \text{ J/K}\cdot\text{mol})(298.15 \text{ K})} = -32.6058655$$

$$\log K = \log (e^{\ln K}) = \log (e^{-32.6058655}) = -14.16$$



Derivation:

$$\Delta G^\circ = \Delta_f G^\circ(\text{Pu}^{4+}) + \Delta_f G^\circ(\text{e}^-) - \Delta_f G^\circ(\text{Pu}^{3+})$$

$$\Delta_f G^\circ(\text{Pu}^{4+}) = -477.988 \text{ kJ/mol}^{\text{d}}$$

$$\Delta_f G^\circ(\text{Pu}^{3+}) = -578.984 \text{ kJ/mol}^{\text{d}}$$

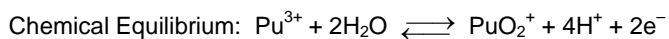
$$\Delta_f G^\circ(\text{e}^-) = 0.000 \text{ kJ/mol}$$

Therefore:

$$\begin{aligned}\Delta G^\circ &= -477.988 - (-578.984) - (0.000) \text{ kJ/mol} \\ &= 100.996 \text{ kJ/mol}\end{aligned}$$

$$\ln K = -\frac{\Delta G^\circ}{RT} = -\frac{(100.996 \text{ kJ/mol})(1000 \text{ J/kJ})}{(8.314510 \text{ J/K}\cdot\text{mol})(298.15 \text{ K})} = -40.7410952$$

$$\log K = \log (e^{\ln K}) = \log (e^{-40.7410952}) = -17.69$$



Derivation:

$$\Delta G^\circ = \Delta_f G^\circ(\text{PuO}_2^+) + 4\Delta_f G^\circ(\text{H}^+) + 2\Delta_f G^\circ(\text{e}^-) - \Delta_f G^\circ(\text{Pu}^{3+}) - 2\Delta_f G^\circ(\text{H}_2\text{O})$$

$$\Delta_f G^\circ(\text{PuO}_2^+) = -852.646 \text{ kJ/mol}^d$$

$$\Delta_f G^\circ(\text{H}^+) = 0.000 \text{ kJ/mol}^e$$

$$\Delta_f G^\circ(\text{e}^-) = 0.000 \text{ kJ/mol}$$

$$\Delta_f G^\circ(\text{Pu}^{3+}) = -578.984 \text{ kJ/mol}^d$$

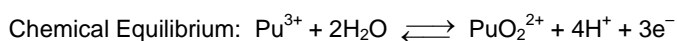
$$\Delta_f G^\circ(\text{H}_2\text{O}) = -237.140 \text{ kJ/mol}^e$$

Therefore:

$$\begin{aligned}\Delta G^\circ &= -852.646 + 4(0.000) + 2(0.000) - (-578.984) - 2(-237.140) \text{ kJ/mol} \\ &= 200.618 \text{ kJ/mol}\end{aligned}$$

$$\ln K = -\frac{\Delta G^\circ}{RT} = -\frac{(200.618 \text{ kJ/mol})(1000 \text{ J/kJ})}{(8.314510 \text{ J/K}\cdot\text{mol})(298.15 \text{ K})} = -80.9279283$$

$$\log K = \log (e^{\ln K}) = \log (e^{-80.9279283}) = -35.15$$



Derivation:

$$\Delta G^\circ = \Delta_f G^\circ(\text{PuO}_2^{2+}) + 4\Delta_f G^\circ(\text{H}^+) + 3\Delta_f G^\circ(\text{e}^-) - \Delta_f G^\circ(\text{Pu}^{3+}) - 2\Delta_f G^\circ(\text{H}_2\text{O})$$

$$\Delta_f G^\circ(\text{PuO}_2^{2+}) = -762.353 \text{ kJ/mol}^d$$

$$\Delta_f G^\circ(\text{H}^+) = 0.000 \text{ kJ/mol}^e$$

$$\Delta_f G^\circ(\text{e}^-) = 0.000 \text{ kJ/mol}$$

$$\Delta_f G^\circ(\text{Pu}^{3+}) = -578.984 \text{ kJ/mol}^d$$

$$\Delta_f G^\circ(\text{H}_2\text{O}) = -237.140 \text{ kJ/mol}^e$$

Therefore:

$$\begin{aligned}\Delta G^\circ &= -762.353 + 4(0.000) + 3(0.000) - (-578.984) - 2(-237.140) \text{ kJ/mol} \\ &= 290.911 \text{ kJ/mol}\end{aligned}$$

$$\ln K = -\frac{\Delta G^\circ}{RT} = -\frac{(290.911 \text{ kJ/mol})(1000 \text{ J/kJ})}{(8.314510 \text{ J/K}\cdot\text{mol})(298.15 \text{ K})} = -117.3515066$$

$$\log K = \log (e^{\ln K}) = \log (e^{-117.3515066}) = -50.97$$

^aTable 8–2 of ref 15.

^bTable 5–2 of ref 15.

^cCalculated elsewhere in this Appendix.

^dTable 5–1 of ref 15.

^eTable 8–1 of ref 15.